

KLH[®]

MADE FOR BUILDING
BUILT FOR LIVING

STRUCTURAL PRE-ANALYSIS TABLES



IMPRINT

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STRUCTURAL PRE-ANALYSIS TABLES

The calculation model for KLH® solid wood panels must consider the influence of the layup (thickness, material, orientation), the internal stress distributions and local stress concentrations. Due to the shear flexible transverse layers, shear deformation may no longer be disregarded and the layup of the panel has to be taken into account.

Dimensioning and structural design follow Eurocode 5 (EN 1995-1-1 and EN 1995-1-2), taking into account the national standards set forth in ÖNORM B 1995-1-1 and ÖNORM B 1995-1-2. It should be pointed out that the national standards in various European countries differ from each other in some detailed aspects (e.g. different partial factors γ_M for “cross laminated timber” material). The material properties of KLH® solid wood panels required for structural design can be taken from the European Technical Assessment (ETA-06/0138).

The structural design of KLH® solid wood panels has to be carried out project-based and locally applicable standards and regulations have to be taken into account.

Due care is also advised when comparing panel thicknesses of KLH® elements with products from other manufacturers: due to different production processes, the cross laminated timber products may well have different properties, e.g. with respect to bending stiffness or shear strength. Please mind the relevant properties in the respective product approvals and take into account the differences in a comparative analysis.

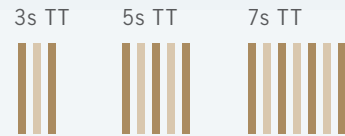
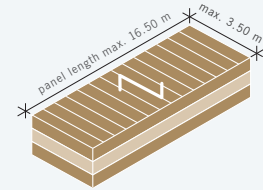
For the structural analysis of cross laminated timber, different models have been developed in the past. The structural analysis of KLH® solid wood panels is based on the shear-elastic beam theory (according to Timoshenko) or the shear-elastic orthotropic plate (according to Reissner-Mindlin). The properties of the composite cross section are thereby described appropriately. To receive correct results (internal forces and moments as well as deformations) is the use of suitable software for the purpose of structural analysis. The software provided on the website by KLH Massivholz GmbH is based on the above mentioned theory and thus a good choice.

STANDARD PANELS AND PANEL STRUCTURES

01 KLH® STANDARD PANEL TYPES AND STRUCTURES

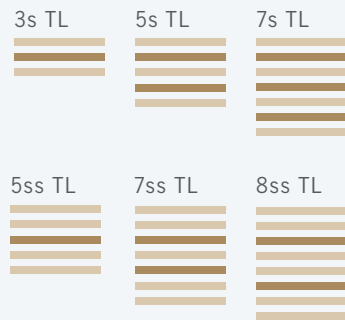
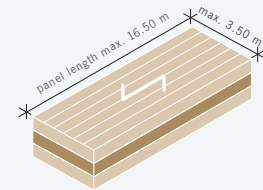
FOR THE WALL
Covering layer in the transverse panel direction TT

| Nominal thickness | Layers | Type | Lamella structure in [mm] | | | | | | | | |
|-------------------|--------|------|---------------------------|----|----|----|----|---|---|---|---|
| | | | T | L | T | L | T | L | T | L | T |
| KLH 60 mm | 3s | TT | 20 | 20 | 20 | | | | | | |
| KLH 70 mm | 3s | TT | 20 | 30 | 20 | | | | | | |
| KLH 80 mm | 3s | TT | 30 | 20 | 30 | | | | | | |
| KLH 90 mm | 3s | TT | 30 | 30 | 30 | | | | | | |
| KLH 100 mm | 3s | TT | 30 | 40 | 30 | | | | | | |
| KLH 110 mm | 3s | TT | 40 | 30 | 40 | | | | | | |
| KLH 120 mm | 3s | TT | 40 | 40 | 40 | | | | | | |
| KLH 100 mm | 5s | TT | 20 | 20 | 20 | 20 | 20 | | | | |
| KLH 110 mm | 5s | TT | 20 | 20 | 30 | 20 | 20 | | | | |
| KLH 120 mm | 5s | TT | 30 | 20 | 20 | 20 | 30 | | | | |
| KLH 130 mm | 5s | TT | 30 | 20 | 30 | 20 | 30 | | | | |
| KLH 140 mm | 5s | TT | 30 | 20 | 40 | 20 | 30 | | | | |
| KLH 150 mm | 5s | TT | 30 | 30 | 30 | 30 | 30 | | | | |
| KLH 160 mm | 5s | TT | 40 | 20 | 40 | 20 | 40 | | | | |



FOR CEILING AND ROOF
Covering layer in the longitudinal panel direction TL

| Nominal thickness | Layers | Type | Lamella structure in [mm] | | | | | | | | |
|-------------------|--------|------|---------------------------|----|-------|----|-------|----|----|---|---|
| | | | L | T | L | T | L | T | L | T | L |
| KLH 60 mm | 3s | TL | 20 | 20 | 20 | | | | | | |
| KLH 70 mm | 3s | TL | 20 | 30 | 20 | | | | | | |
| KLH 80 mm | 3s | TL | 30 | 20 | 30 | | | | | | |
| KLH 90 mm | 3s | TL | 30 | 30 | 30 | | | | | | |
| KLH 100 mm | 3s | TL | 40 | 20 | 40 | | | | | | |
| KLH 110 mm | 3s | TL | 40 | 30 | 40 | | | | | | |
| KLH 120 mm | 3s | TL | 40 | 40 | 40 | | | | | | |
| KLH 100 mm | 5s | TL | 20 | 20 | 20 | 20 | 20 | | | | |
| KLH 110 mm | 5s | TL | 20 | 20 | 30 | 20 | 20 | | | | |
| KLH 120 mm | 5s | TL | 30 | 20 | 20 | 20 | 30 | | | | |
| KLH 130 mm | 5s | TL | 30 | 20 | 30 | 20 | 30 | | | | |
| KLH 140 mm | 5s | TL | 40 | 20 | 20 | 20 | 40 | | | | |
| KLH 150 mm | 5s | TL | 40 | 20 | 30 | 20 | 40 | | | | |
| KLH 160 mm | 5s | TL | 40 | 20 | 40 | 20 | 40 | | | | |
| KLH 170 mm | 5s | TL | 40 | 30 | 30 | 30 | 40 | | | | |
| KLH 180 mm | 5s | TL | 40 | 30 | 40 | 30 | 40 | | | | |
| KLH 190 mm | 5s | TL | 40 | 40 | 30 | 40 | 40 | | | | |
| KLH 200 mm | 5s | TL | 40 | 40 | 40 | 40 | 40 | | | | |
| KLH 160 mm | 5ss | TL | 30+30 | 40 | 30+30 | | | | | | |
| KLH 180 mm | 7s | TL | 20 | 40 | 20 | 20 | 20 | 40 | 20 | | |
| KLH 200 mm | 7s | TL | 20 | 40 | 20 | 40 | 20 | 40 | 20 | | |
| KLH 220 mm | 7s | TL | 30 | 40 | 30 | 20 | 30 | 40 | 30 | | |
| KLH 240 mm | 7s | TL | 30 | 40 | 30 | 40 | 30 | 40 | 30 | | |
| KLH 180 mm | 7ss | TL | 30+30 | 20 | 20 | 20 | 30+30 | | | | |
| KLH 200 mm | 7ss | TL | 30+30 | 20 | 40 | 20 | 30+30 | | | | |
| KLH 220 mm | 7ss | TL | 40+40 | 20 | 20 | 20 | 40+40 | | | | |
| KLH 240 mm | 7ss | TL | 40+40 | 20 | 40 | 20 | 40+40 | | | | |
| KLH 260 mm | 7ss | TL | 40+40 | 30 | 40 | 30 | 40+40 | | | | |
| KLH 280 mm | 7ss | TL | 40+40 | 40 | 40 | 40 | 40+40 | | | | |
| KLH 300 mm | 8ss | TL | 40+40 | 30 | 40+40 | 30 | 40+40 | | | | |
| KLH 320 mm | 8ss | TL | 40+40 | 40 | 40+40 | 40 | 40+40 | | | | |



Special panel layouts are available on request. By using double layers, for example the longitudinal or transverse stiffness of the panel can be further enhanced. The fire resistance of the KLH® solid wood panel can also be influenced by modifying the structures and can eventually be improved in relation to specific project requirements.

Invoicing widths

2.45 | 2.50 | 2.73 | 2.95 |
3.10 | 3.20 | 3.30 | 3.40 | 3.50 [m]

Maximum length 16.50 [m]

Maximum thickness 0.5 [m]

STRUCTURAL PRE-ANALYSIS TABLES

02 KLH® AS A VISIBLE WALL

2.1 SINGLE-SIDED FIRE EXPOSURE (FOR EXTERIOR WALLS)

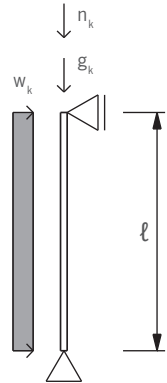
according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Wind pressure: $w_k = 0,8 \text{ kN/m}^2$

Minimum panel thickness for various fire resistance classes (R 0 to R 90)



| Permanent load | Imposed load | HEIGHT WALL (buckling length ℓ) | | | | | | | |
|----------------|--------------|---------------------------------------|----------|-----------|-----------|----------|-----------|-----------|-----------|
| | | 2,73 m | | | | 2,95 m | | | |
| $g_{2,k}$ | n_k | R 0 | R 30 | R 60 | R 90 | R 0 | R 30 | R 60 | R 90 |
| [kN/m] | [kN/m] | | | | | | | | |
| 10,00 | 10,00 | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 120 TT | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 120 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 20,00 | 10,00 | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 120 TT | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 120 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 30,00 | 10,00 | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 120 TT | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 120 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 40,00 | 10,00 | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 130 TT | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 130 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 50,00 | 10,00 | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 130 TT | 3s 60 TT | 3s 80 TT | 5s 100 TT | 5s 130 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 60,00 | 10,00 | 3s 60 TT | 3s 90 TT | 5s 100 TT | 5s 130 TT | 3s 70 TT | 3s 90 TT | 5s 100 TT | 5s 130 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 60,00 | 10,00 | 3s 70 TT | 3s 90 TT | 5s 100 TT | 5s 130 TT | 3s 70 TT | 3s 100 TT | 5s 110 TT | 5s 130 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 60,00 | 10,00 | 3s 70 TT | 3s 90 TT | 5s 100 TT | 5s 130 TT | 3s 80 TT | 3s 100 TT | 5s 110 TT | 5s 130 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |

R 0

R 30

R 60

R 90

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

Imposed load category A ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{\text{mod}} = 0,8$

Wind loads ($\psi_0 = 0,6$ and $\psi_2 = 0,0$): $k_{\text{mod}} = 1,0$

Self-weight of KLH® is already taken into account in the table.

Load-bearing capacity

- a) verification of column stability (compression and deflection according to equivalent member method)
- b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

- a) charring rate $\beta_1 = 0,55$ mm/min regular charring rate (charring within one single layer)
- b) charring rate $\beta_2 = 0,80$ mm/min increased charring rate (after the failure / falling off of one layer)
- c) for local panel parts $b < 300$ mm higher charring rates are mandatory
- d) additional eccentricity due to burn-off taken into account

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

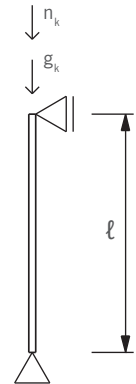
2.2 DOUBLE-SIDED FIRE EXPOSURE (FOR INTERIOR WALLS)

according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Minimum panel thickness for various fire resistance classes (R 0 to R 60)



| Permanent load | Imposed load | HEIGHT WALL (buckling length ℓ) | | | | | | |
|----------------|--------------|---------------------------------------|-----------|-----------|----------|-----------|-----------|-----------|
| | | 2,73 m | | | 2,95 m | | | |
| $g_{2,k}$ | n_k | R 0 | R 30 | R 60 | R 0 | R 30 | R 60 | |
| [kN/m] | [kN/m] | | | | | | | |
| 10,00 | 10,00 | 3s 60 TT | 3s 80 TT | 7s 180 TT | 3s 60 TT | 3s 80 TT | 7s 180 TT | |
| | 20,00 | | | | | 3s 90 TT | | |
| | 30,00 | | | | | | | |
| | 40,00 | | | | | | | |
| | 50,00 | | | | | | | |
| 60,00 | | | | | | | | |
| 20,00 | 10,00 | 3s 60 TT | 3s 80 TT | 7s 180 TT | 3s 60 TT | 3s 90 TT | 7s 180 TT | |
| | 20,00 | | 3s 90 TT | | | | | |
| | 30,00 | | | | | | | |
| | 40,00 | | | | | | | |
| | 50,00 | | | | | | | |
| 60,00 | 3s 70 TT | | | | | | | |
| 30,00 | 10,00 | 3s 60 TT | 3s 90 TT | 7s 180 TT | 3s 60 TT | 3s 90 TT | 7s 180 TT | |
| | 20,00 | | | | | | | 3s 100 TT |
| | 30,00 | | | | | | | |
| | 40,00 | | | | | | | |
| | 50,00 | | | | | | | |
| 60,00 | 3s 70 TT | | | | | | | |
| 40,00 | 10,00 | 3s 60 TT | 3s 90 TT | 7s 180 TT | 3s 60 TT | 3s 100 TT | 7s 180 TT | |
| | 20,00 | | 3s 100 TT | | | | | |
| | 30,00 | | | | | | | |
| | 40,00 | | | | | | | |
| | 50,00 | | | | | | | |
| 60,00 | 3s 70 TT | | | | | | | |
| 50,00 | 10,00 | 3s 60 TT | 3s 100 TT | 7s 180 TT | 3s 60 TT | 3s 100 TT | 7s 180 TT | |
| | 20,00 | | | | | | | 3s 110 TT |
| | 30,00 | | | | | | | |
| | 40,00 | | | | | | | |
| | 50,00 | | | | | | | |
| 60,00 | 3s 70 TT | | | | | | | |
| 60,00 | 10,00 | 3s 60 TT | 3s 100 TT | 7s 180 TT | 3s 70 TT | 3s 110 TT | 7s 180 TT | |
| | 20,00 | | 3s 110 TT | | | | | |
| | 30,00 | | | | | | | |
| | 40,00 | | | | | | | |
| | 50,00 | | | | | | | |
| 60,00 | 3s 70 TT | | | | | | | |
| | | | | | 3s 80 TT | | | |

R 0

R 30

R 60

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

Imposed load category A ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$
Self-weight of KLH® is already taken into account in the table.

Load-bearing capacity

a) verification of column stability (compression and deflection according to equivalent member method)

Structural fire design (double-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

- a) charring rate $\beta_1 = 0,55$ mm/min regular charring rate (charring within one single layer)
- b) charring rate $\beta_2 = 0,80$ mm/min increased charring rate (after the failure / falling off of one layer)
- c) for local panel parts $b < 300$ mm higher charring rates are mandatory

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

03 KLH® AS A CLADDED WALL

3.1 SINGLE-SIDED FIRE EXPOSURE (FOR EXTERIOR WALLS)

according to ETA-06/0138

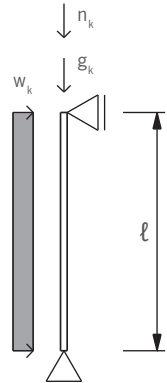
ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Wind pressure: $w_k = 0,8 \text{ kN/m}^2$

Minimum panel thickness for various fire resistance classes (R 30 to R 120)

with 15 mm fire rated gypsum plasterboard type F (GtF) on the fire exposed side



| Permanent load | Imposed load | HEIGHT WALL (buckling length ℓ) | | | | | | | |
|----------------|--------------|---------------------------------------|----------|-----------|-----------|----------|----------|-----------|-----------|
| | | 2,73 m | | | | 2,95 m | | | |
| $g_{2,k}$ | n_k | R 30 | R 60 | R 90 | R 120 | R 30 | R 60 | R 90 | R 120 |
| [kN/m] | [kN/m] | | | | | | | | |
| 10,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 110 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 110 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 20,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 110 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 110 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 30,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 110 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 110 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 40,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 120 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 120 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 50,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 120 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 120 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 60,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 120 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 5s 120 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 60,00 | | | | | | | | | |

R 30

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

Imposed load category A ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{\text{mod}} = 0,8$

Wind loads ($\psi_0 = 0,6$ and $\psi_2 = 0,0$): $k_{\text{mod}} = 1,0$

Self-weight of KLH® is already taken into account in the table.

Load-bearing capacity

- a) verification of column stability (compression and deflection according to equivalent member method)
- b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

- a) charring rate $\beta_1 = 0,55$ mm/min regular charring rate (charring within one single layer)
- b) charring rate $\beta_2 = 0,80$ mm/min increased charring rate (after the failure / falling off of one layer)
- c) for local panel parts $b < 300$ mm higher charring rates are mandatory
- d) additional eccentricity due to burn-off taken into account

Cladding

For the cladding directly to the KLH® surface, screw-fastened fire rated gypsum plasterboards type F (GtF according to ÖNORM EN 520 and ÖNORM B 3410 or DIN 18180) or equivalent panels are required. The fastening needs to comply with the state of the art and the current KLH® installation guidelines.

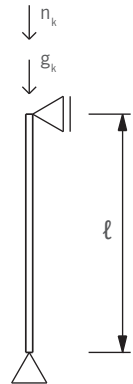
This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

3.2 DOUBLE-SIDED FIRE EXPOSURE (FOR INTERIOR WALLS)

according to ETA-06/0138
 ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019
 ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Minimum panel thickness for various fire resistance classes (R 30 to R 120)
 with 15 mm fire rated gypsum plasterboard type F (GtF) on both sides



| Permanent load | Imposed load | HEIGHT WALL (buckling length ℓ) | | | | | | | |
|----------------|--------------|---------------------------------------|----------|-----------|-----------|----------|----------|-----------|-----------|
| | | 2,73 m | | | | 2,95 m | | | |
| $g_{2,k}$ | n_k | R 30 | R 60 | R 90 | R 120 | R 30 | R 60 | R 90 | R 120 |
| [kN/m] | [kN/m] | | | | | | | | |
| 10,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 20,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 30,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 40,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 50,00 | 10,00 | 3s 80 TT | 3s 80 TT | 3s 120 TT | 3s 100 TT | 3s 80 TT | 3s 90 TT | 3s 120 TT | 3s 100 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |
| 60,00 | 10,00 | 3s 80 TT | 3s 90 TT | 3s 120 TT | 3s 100 TT | 3s 80 TT | 3s 90 TT | 3s 80 TT | 3s 100 TT |
| | 20,00 | | | | | | | | |
| | 30,00 | | | | | | | | |
| | 40,00 | | | | | | | | |
| | 50,00 | | | | | | | | |

with 1 x 15 mm GtF on both sides



with 2 x 15 mm GtF on both sides



STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

Imposed load category A ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{\text{mod}} = 0,8$
Self-weight of KLH® is already taken into account in the table.

Load-bearing capacity

a) verification of column stability (compression and deflection according to equivalent member method)

Structural fire design (double-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

- a) charring rate $\beta_1 = 0,55$ mm/min regular charring rate (charring within one single layer)
- b) charring rate $\beta_2 = 0,80$ mm/min increased charring rate (after the failure / falling off of one layer)
- c) for local panel parts $b < 300$ mm higher charring rates are mandatory

Cladding

For the cladding directly to the KLH® surface, screw-fastened fire rated gypsum plasterboards type F (GtF according to ÖNORM EN 520 and ÖNORM B 3410 or DIN 18180) or equivalent panels are required. The fastening needs to comply with the state of the art and the current KLH® installation guidelines.

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

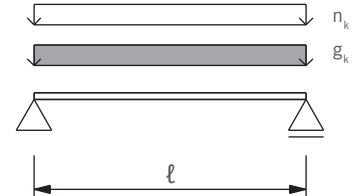
04 KLH® AS A FLOOR - SINGLE-SPAN BEAM

4.1 VERIFICATION OF VIBRATION WITH HIGH REQUIREMENTS (WET SCREED)

according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011



Minimum panel thickness for a specific load-span-combination

| Permanent load $g_{2,k}$ | Imposed load n_k | | SPAN OF SINGLE-SPAN BEAM l | | | | |
|-----------------------------|-----------------------|----------------------|------------------------------|-----------|-----------|------------|------------|
| | category | [kN/m ²] | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m |
| 1,00 | A | 1,50 | 5s 120 TL | 5s 140 TL | 5s 170 TL | 7s 220 TL | 7s 240 TL |
| | | 2,00 | | | | | |
| | | 2,80 | | | | | |
| | B | 3,00 | | 5s 140 TL | | 7ss 260 TL | |
| | | 3,50 | | | | | |
| | | 4,00 | | | | | |
| 1,50 | A | 1,50 | 5s 120 TL | 5s 140 TL | 5s 170 TL | 7s 220 TL | 7s 240 TL |
| | | 2,00 | | | | | |
| | | 2,80 | | | | | |
| | B | 3,00 | | 5s 140 TL | | 7ss 260 TL | |
| | | 3,50 | | | | | |
| | | 4,00 | | | | | |
| 2,00 | A | 1,50 | 5s 120 TL | 5s 140 TL | 5s 180 TL | 7s 220 TL | 7s 240 TL |
| | | 2,00 | | | | | |
| | | 2,80 | | | | | |
| | B | 3,00 | | 5s 140 TL | | 7ss 280 TL | |
| | | 3,50 | | | | | |
| | | 4,00 | | | | | |
| 2,50 | A | 1,50 | 5s 120 TL | 5s 140 TL | 5s 200 TL | 7s 220 TL | 7s 240 TL |
| | | 2,00 | | | | | |
| | | 2,80 | | | | | |
| | B | 3,00 | | | | 7ss 280 TL | |
| | | 3,50 | | | | | |
| | | 4,00 | | | | | |
| 3,00 | A | 1,50 | 5s 120 TL | 5s 150 TL | 5s 200 TL | 7s 220 TL | 7ss 280 TL |
| | | 2,00 | | | | | |
| | | 2,80 | | | | | |
| | B | 3,00 | | | | 7s 240 TL | |
| | | 3,50 | | | | | |
| | | 4,00 | | | | | |
| C | 4,00 | 7ss 260 TL | | | | | |
| | 5,00 | | | | | | |

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$$k_{def} = 0,6$$

Imposed load category A and B ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$

Imposed load category C ($\psi_0 = 0,7$ and $\psi_2 = 0,6$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Vibration verification according to ÖNORM B 1995-1-1:2019

a) floor slab class I: slab between different utilisation units (e.g. separating floor slabs for apartments or offices);
6 cm wet screed, floating on filler

b) limiting value of the frequency and stiffness criterion: $f_{1,min} \geq 4,5$ Hz; $f_1 \geq f_{gr} = 8$ Hz; $w_{stat} \leq w_{gr} = 0,25$ mm

c) modal damping ratio for cross-laminated timber floor slabs with floating screed and heavy floor structure: $\zeta = 4,0$ %

d) limiting value acceleration (required at $f_{1,min} \leq f_1 \leq f_{gr}$): $\alpha_{rms} \leq \alpha_{gr} = 0,05$ m/s²

e) floor slab width (b) $\leq 1,2 \cdot \text{span}$ (1,2*1)

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduces properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

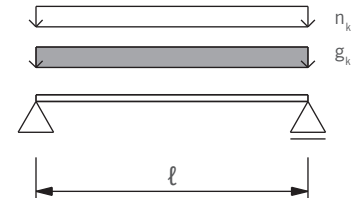
4.2 VERIFICATION OF VIBRATION WITH HIGH REQUIREMENTS (DRY SCREED)

according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Minimum panel thickness for a specific load-span-combination



| Permanent load $g_{2,k}$ | Imposed load n_k | | SPAN OF SINGLE-SPAN BEAM l | | | | | | | | | |
|-----------------------------|-----------------------|----------------------|------------------------------|-----------|------------|------------|------------|-----------|-----------|-----------|------------|------------|
| | category | [kN/m ²] | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | | | | | |
| 1,00 | A | 1,50 | 5s 130 TL | 5s 150 TL | 5s 170 TL | 7s 220 TL | 7ss 280 TL | | | | | |
| | | 2,00 | | | | | | | | | | |
| | | 2,80 | | | | | | | | | | |
| | B | 3,00 | | | | | | | | | | |
| | | 3,50 | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | |
| | C | 5,00 | | | | | | | | | | |
| | | 1,50 | | | | | | 5s 130 TL | 5s 150 TL | 5s 180 TL | 7s 220 TL | 7ss 280 TL |
| | | 2,00 | | | | | | | | | | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | 7s 240 TL | | | | | | | | | | |
| | 1,50 | 5s 130 TL | 5s 150 TL | 5s 190 TL | 7s 240 TL | 7ss 280 TL | | | | | | |
| | 2,00 | | | | | | | | | | | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | | | | | | | | | | | |
| | 1,50 | | | | | | 5s 130 TL | 5s 150 TL | 5s 200 TL | 7s 240 TL | 7ss 280 TL | |
| | 2,00 | | | | | | | | | | | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | | | | | | | | | | | |
| | 1,50 | 5s 130 TL | 5s 150 TL | 5s 200 TL | 7s 240 TL | 7ss 280 TL | | | | | | |
| | 2,00 | | | | | | | | | | | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | | | | 7ss 260 TL | | | | | | | |

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$$k_{def} = 0,6$$

Imposed load category A and B ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$

Imposed load category C ($\psi_0 = 0,7$ and $\psi_2 = 0,6$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Vibration verification according to ÖNORM B 1995-1-1:2019

a) floor slab class I: slab between different utilisation units (e.g. separating floor slabs for apartments or offices);
dry screed, floating on heavy filler (at least 60 kg/m²)

b) limiting value of the frequency and stiffness criterion: $f_{1,min} \geq 4,5$ Hz; $f_1 \geq f_{gr} = 8$ Hz; $w_{stat} \leq w_{gr} = 0,25$ mm

c) modal damping ratio for cross-laminated timber floor slabs with floating screed and heavy floor structure: $\zeta = 4,0$ %

d) limiting value acceleration (required at $f_{1,min} \leq f_1 \leq f_{gr}$): $\alpha_{rms} \leq \alpha_{gr} = 0,05$ m/s²

e) floor slab width (b) $\leq 1,2 \cdot \text{span}$ (1,2*1)

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

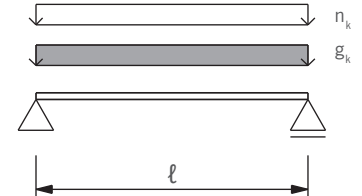
STRUCTURAL PRE-ANALYSIS TABLES

4.3 VERIFICATION OF VIBRATION WITH LOW REQUIREMENTS

according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011



Minimum panel thickness for a specific load-span-combination

| Permanent load | Imposed load | | SPAN OF SINGLE-SPAN BEAM l | | | | | | |
|----------------|-----------------------------------|-------------------------------------------|------------------------------|-----------|-----------|------------|------------|-----------|------------|
| | $g_{2,k}$ [kN/m ²] | n_k category [kN/m ²] | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | | |
| 1,00 | A | 1,50 | 5s 100 TL | 5s 120 TL | 5s 150 TL | 5s 160 TL | 5s 200 TL | | |
| | | 2,00 | | | | 5s 170 TL | | | |
| | | 2,80 | | | | | | | |
| | B | 3,00 | | 5s 130 TL | 5s 160 TL | 5s 190 TL | 7ss 220 TL | | |
| | | 3,50 | | | | | | | |
| | C | 4,00 | | 5s 140 TL | 5s 170 TL | 7ss 200 TL | | | |
| | | 5,00 | | | | | | | |
| | 1,50 | A | | 1,50 | 5s 100 TL | 5s 120 TL | 5s 150 TL | 5s 180 TL | 5s 200 TL |
| | | | | 2,00 | | | | 5s 200 TL | |
| 2,80 | | | | | | | | | |
| B | | 3,00 | 5s 130 TL | 5s 160 TL | | 5s 200 TL | 7ss 220 TL | | |
| | | 3,50 | | | | | | | |
| C | | 4,00 | 5s 140 TL | 5s 170 TL | | 7ss 200 TL | 7ss 240 TL | | |
| | | 5,00 | | | | | | | |
| 2,00 | | A | 1,50 | 5s 100 TL | | 5s 120 TL | 5s 150 TL | 5s 190 TL | 7ss 240 TL |
| | | | 2,00 | | | | | | |
| | 2,80 | | | | | | | | |
| | B | 3,00 | 5s 130 TL | | 5s 170 TL | 7ss 200 TL | | | |
| | | 3,50 | | | | | | | |
| | C | 4,00 | 5s 110 TL | | 5s 140 TL | 5s 180 TL | | | |
| | | 5,00 | | | | | | | |
| | 2,50 | A | 1,50 | | 5s 100 TL | 5s 130 TL | 5s 160 TL | 5s 190 TL | 7ss 240 TL |
| | | | 2,00 | | | | | | |
| 2,80 | | | | | | | | | |
| B | | 3,00 | 5s 140 TL | 5s 180 TL | | 5s 200 TL | | | |
| | | 3,50 | | | | | | | |
| C | | 4,00 | 5s 110 TL | 5s 140 TL | | 5s 180 TL | 7ss 220 TL | | |
| | | 5,00 | | | | | | | |
| 3,00 | | A | 1,50 | 5s 100 TL | | 5s 130 TL | 5s 160 TL | 5s 200 TL | 7ss 240 TL |
| | | | 2,00 | | | | | | |
| | 2,80 | | | | | | | | |
| | B | 3,00 | 5s 140 TL | | 5s 180 TL | 7ss 220 TL | | | |
| | | 3,50 | | | | | | | |
| | C | 4,00 | 5s 110 TL | | 5s 140 TL | 5s 190 TL | 7ss 260 TL | | |
| | | 5,00 | | | | | | | |

R 30

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$$k_{def} = 0,6$$

Imposed load category A and B ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$

Imposed load category C ($\psi_0 = 0,7$ and $\psi_2 = 0,6$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Vibration verification according to ÖNORM B 1995-1-1:2019

a) floor slab class II: slab within the utilisation unit (e.g. detached house); floating wet screed (even without filler); dry screed, floating on heavy filler (at least 60 kg/m²)

b) limiting value of the frequency and stiffness criterion: $f_{1,min} \geq 4,5$ Hz; $f_1 \geq f_{gr} = 6$ Hz; $w_{stat} \leq w_{gr} = 0,50$ mm

c) modal damping ratio for cross-laminated timber floor slabs with floating screed and heavy floor structure: $\zeta = 4,0$ %

d) limiting value acceleration (required at $f_{1,min} \leq f_1 \leq f_{gr}$): $\alpha_{rms} \leq \alpha_{gr} = 0,10$ m/s²

e) floor slab width $(b) \leq 1,2 \cdot \text{span}$ (1,2*1)

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

05 KLH® AS A FLOOR - DOUBLE-SPAN BEAM

5.1 VERIFICATION OF VIBRATION WITH HIGH REQUIREMENTS (WET SCREED)

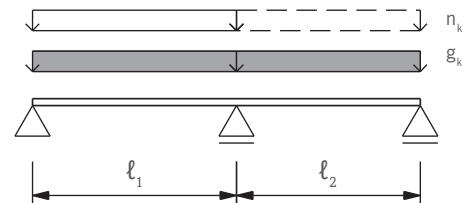
according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Imposed load not favourable in some spans

Minimum panel thickness for a specific load-span-combination



| Permanent load $g_{2,k}$ | Imposed load n_k | | SPAN OF DOUBLE-SPAN BEAM l_1 | | | | | | | | | |
|-----------------------------|-----------------------|----------------------|--------------------------------|-----------|-----------|-----------|------------|-----------|-----------|-----------|------------|-----------|
| | category | [kN/m ²] | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | | | | | |
| 1,00 | A | 1,50 | 5s 110 TL | 5s 130 TL | 5s 150 TL | 5s 180 TL | 7s 200 TL | | | | | |
| | | 2,00 | | | | | 7ss 220 TL | | | | | |
| | | 2,80 | | | | | | | | | | |
| | B | 3,00 | | | | | 7ss 220 TL | | | | | |
| | | 3,50 | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | |
| | C | 5,00 | | | | | 7ss 220 TL | | | | | |
| | | 1,50 | | | | | | 5s 110 TL | 5s 130 TL | 5s 160 TL | 5s 180 TL | 7s 200 TL |
| | | 2,00 | | | | | | | | | | 7s 220 TL |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | 7s 220 TL | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | 7s 220 TL | | | | | | | | | | |
| | 1,50 | | 5s 110 TL | 5s 130 TL | 5s 160 TL | 5s 190 TL | 7s 240 TL | | | | | |
| | 2,00 | | | | | | 7s 220 TL | | | | | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | 7s 220 TL | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | 7s 240 TL | | | | | | | | | | |
| | 1,50 | | | | | | 5s 110 TL | 5s 130 TL | 5s 160 TL | 5s 190 TL | 7s 220 TL | |
| | 2,00 | | | | | | | | | | 7s 240 TL | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | 7s 240 TL | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | 7s 240 TL | | | | | | | | | | |
| | 1,50 | | 5s 110 TL | 5s 130 TL | 5s 160 TL | 5s 190 TL | | | | | 7ss 240 TL | |
| | 2,00 | | | | | | | | | | 7ss 240 TL | |
| 2,80 | | | | | | | | | | | | |
| B | 3,00 | 7ss 240 TL | | | | | | | | | | |
| | 3,50 | | | | | | | | | | | |
| | 4,00 | | | | | | | | | | | |
| C | 5,00 | 7ss 240 TL | | | | | | | | | | |

R 30

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$$k_{def} = 0,6$$

Imposed load category A and B ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$

Imposed load category C ($\psi_0 = 0,7$ and $\psi_2 = 0,6$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Vibration verification according to ÖNORM B 1995-1-1:2019

a) floor slab class I: slab between different utilisation units (e.g. separating floor slabs for apartments or offices);
6 cm wet screed, floating on filler

b) limiting value of the frequency and stiffness criterion: $f_{1,min} \geq 4,5$ Hz; $f_1 \geq f_{gr} = 8$ Hz; $w_{stat} \leq w_{gr} = 0,25$ mm

c) modal damping ratio for cross-laminated timber floor slabs with floating screed and heavy floor structure: $\zeta = 4,0$ %

d) limiting value acceleration (required at $f_{1,min} \leq f_1 \leq f_{gr}$): $\alpha_{rms} \leq \alpha_{gr} = 0,05$ m/s²

e) floor slab width (b) $\leq 1,2 \cdot \text{span}$ (1,2*1)

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

5.2 VERIFICATION OF VIBRATION WITH HIGH REQUIREMENTS (DRY SCREED)

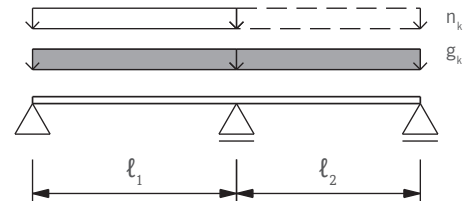
according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Imposed load not favourable in some spans

Minimum panel thickness for a specific load-span-combination



| Permanent load $g_{2,k}$ | Imposed load n_k | | SPAN OF DOUBLE-SPAN BEAM l_1 | | | | | | | | | | |
|-----------------------------|-----------------------|----------------------|--------------------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| | category | [kN/m ²] | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | | | | | | |
| 1,00 | A | 1,50 | 5s 110 TL | 5s 140 TL | 5s 160 TL | 5s 190 TL | 7s 200 TL | | | | | | |
| | | 2,00 | | | | | | 7s 220 TL | | | | | |
| | | 2,80 | | | | | | | | | | | |
| | B | 3,00 | | | | | 5s 140 TL | | 5s 190 TL | 7s 220 TL | | | |
| | | 3,50 | | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | | |
| | C | 4,00 | | | | | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | |
| | | 5,00 | | | | | | | | | | | |
| | | 5,00 | | | | | | | | | | | |
| | 1,50 | A | | | | | 1,50 | 5s 110 TL | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 200 TL | |
| | | | | | | | 2,00 | | | | | | 7s 220 TL |
| | | | | | | | 2,80 | | | | | | |
| B | | 3,00 | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | | | | | |
| | | 3,50 | | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | | |
| C | | 4,00 | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | | | | | |
| | | 5,00 | | | | | | | | | | | |
| | | 5,00 | | | | | | | | | | | |
| 2,00 | | A | 1,50 | 5s 110 TL | 5s 140 TL | 5s 170 TL | 5s 190 TL | | | | | 7s 220 TL | |
| | | | 2,00 | | | | | | | | | | 7s 240 TL |
| | | | 2,80 | | | | | | | | | | |
| | B | 3,00 | 5s 140 TL | | | | | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | |
| | | 3,50 | | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | | |
| | C | 4,00 | 5s 140 TL | | | | | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | |
| | | 5,00 | | | | | | | | | | | |
| | | 5,00 | | | | | | | | | | | |
| | 2,50 | A | 1,50 | | | | | 5s 110 TL | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 220 TL | |
| | | | 2,00 | | | | | | | | | | 7s 240 TL |
| | | | 2,80 | | | | | | | | | | |
| B | | 3,00 | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | | | | | |
| | | 3,50 | | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | | |
| C | | 4,00 | 5s 140 TL | 5s 170 TL | 5s 190 TL | 7s 220 TL | | | | | | | |
| | | 5,00 | | | | | | | | | | | |
| | | 5,00 | | | | | | | | | | | |
| 3,00 | | A | 1,50 | 5s 110 TL | 5s 150 TL | 5s 170 TL | 5s 190 TL | | | | | 7s 240 TL | |
| | | | 2,00 | | | | | | | | | | |
| | | | 2,80 | | | | | | | | | | |
| | B | 3,00 | 5s 110 TL | | | | | 5s 150 TL | 5s 170 TL | 5s 190 TL | 7s 240 TL | | |
| | | 3,50 | | | | | | | | | | | |
| | | 4,00 | | | | | | | | | | | |
| | C | 4,00 | 5s 110 TL | | | | | 5s 150 TL | 5s 170 TL | 5s 190 TL | 7s 240 TL | | |
| | | 5,00 | | | | | | | | | | | |
| | | 5,00 | | | | | | | | | | | |

R 30

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$$k_{def} = 0,6$$

Imposed load category A and B ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$

Imposed load category C ($\psi_0 = 0,7$ and $\psi_2 = 0,6$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Vibration verification according to ÖNORM B 1995-1-1:2019

a) floor slab class I: slab between different utilisation units (e.g. separating floor slabs for apartments or offices);
dry screed, floating on heavy filler (at least 60 kg/m²)

b) limiting value of the frequency and stiffness criterion: $f_{1,min} \geq 4,5$ Hz; $f_1 \geq f_{gr} = 8$ Hz; $w_{stat} \leq w_{gr} = 0,25$ mm

c) modal damping ratio for cross-laminated timber floor slabs with floating screed and heavy floor structure: $\zeta = 4,0$ %

d) limiting value acceleration (required at $f_{1,min} \leq f_1 \leq f_{gr}$): $\alpha_{rms} \leq \alpha_{gr} = 0,05$ m/s²

e) floor slab width ($b \leq 1,2 \cdot \text{span}$ (1,2*1))

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

5.3 VERIFICATION OF VIBRATION WITH LOW REQUIREMENTS

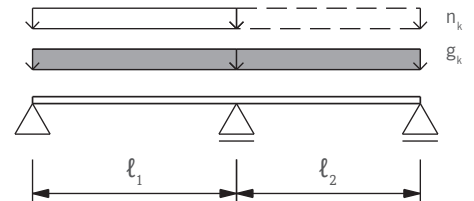
according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Imposed load not favourable in some spans

Minimum panel thickness for a specific load-span-combination



| Permanent load $g_{2,k}$ | Imposed load n_k | | SPAN OF DOUBLE-SPAN BEAM l_1 | | | | | | | |
|-----------------------------|-----------------------|----------------------|--------------------------------|------------|------------|------------|-----------|-----------|-----------|-----------|
| | category | [kN/m ²] | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | | | |
| 1,00 | A | 1,50 | 3s 110 TL | 5s 110 TL | 5s 130 TL | 5s 160 TL | 5s 170 TL | | | |
| | | 2,00 | | | | | | | | |
| | | 2,80 | | | | | | | | |
| | B | 3,00 | | | | | | 5s 110 TL | 5s 140 TL | 5s 180 TL |
| | | 3,50 | | | | | | 5s 120 TL | 5s 200 TL | |
| | | 4,00 | | | | | | 5s 110 TL | 5s 140 TL | |
| | C | 5,00 | | 5s 110 TL | 5s 140 TL | 5s 200 TL | | | | |
| | | 1,50 | | 5s 110 TL | 5s 140 TL | | 5s 180 TL | | | |
| | | 2,00 | | 5s 110 TL | 5s 140 TL | | | | | |
| | B | 2,80 | | 5s 110 TL | 5s 140 TL | 5s 180 TL | | | | |
| | | 3,00 | | 5s 110 TL | 5s 140 TL | | | | | |
| | | 3,50 | | 5s 120 TL | 5s 170 TL | | 5s 200 TL | | | |
| C | 4,00 | 5s 110 TL | 5s 140 TL | 5s 190 TL | | | | | | |
| | 5,00 | 5s 120 TL | 5s 170 TL | | 5s 200 TL | | | | | |
| | 1,50 | 5s 110 TL | 5s 140 TL | | | 5s 190 TL | | | | |
| A | 2,00 | 5s 110 TL | 5s 140 TL | 5s 190 TL | | | | | | |
| | 2,80 | 5s 110 TL | 5s 140 TL | | | | | | | |
| | 3,00 | 5s 120 TL | 5s 170 TL | | 7ss 200 TL | | | | | |
| B | 3,50 | 5s 120 TL | 5s 150 TL | 5s 160 TL | | 5s 200 TL | | | | |
| | 4,00 | 5s 120 TL | 5s 150 TL | | | | | | | |
| | 5,00 | 5s 180 TL | 7ss 200 TL | | | | | | | |
| C | 1,50 | 5s 120 TL | 5s 150 TL | 5s 160 TL | 5s 200 TL | | | | | |
| | 2,00 | 5s 120 TL | 5s 150 TL | | | | | | | |
| | 2,80 | 5s 120 TL | 5s 150 TL | | | 7ss 220 TL | | | | |
| A | 3,00 | 5s 120 TL | 5s 150 TL | 5s 170 TL | 7ss 220 TL | | | | | |
| | 3,50 | 5s 120 TL | 5s 150 TL | | | | | | | |
| | 4,00 | 5s 140 TL | 5s 180 TL | | | 7ss 220 TL | | | | |
| B | 5,00 | 5s 140 TL | 5s 180 TL | 7ss 220 TL | | | | | | |
| | 1,50 | 5s 140 TL | 5s 180 TL | | | | | | | |
| | 2,00 | 5s 140 TL | 5s 180 TL | | | | | | | |

R 30

R 60

R 90

R 120

STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$$k_{def} = 0,6$$

Imposed load category A and B ($\psi_0 = 0,7$ and $\psi_2 = 0,3$): $k_{mod} = 0,8$

Imposed load category C ($\psi_0 = 0,7$ and $\psi_2 = 0,6$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Vibration verification according to ÖNORM B 1995-1-1:2019

a) floor slab class II: slab within the utilisation unit (e.g. detached house); floating wet screed (even without filler); dry screed, floating on heavy filler (at least 60 kg/m²)

b) limiting value of the frequency and stiffness criterion: $f_{1,min} \geq 4,5$ Hz; $f_1 \geq f_{gr} = 6$ Hz; $w_{stat} \leq w_{gr} = 0,50$ mm

c) modal damping ratio for cross-laminated timber floor slabs with floating screed and heavy floor structure: $\zeta = 4,0$ %

d) limiting value acceleration (required at $f_{1,min} \leq f_1 \leq f_{gr}$): $\alpha_{rms} \leq \alpha_{gr} = 0,10$ m/s²

e) floor slab width (b) $\leq 1,2 \cdot \text{span}$ (1,2*1)

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

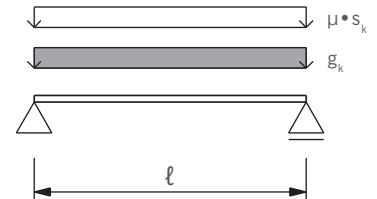
STRUCTURAL PRE-ANALYSIS TABLES

06 KLH® AS A ROOF - SINGLE-SPAN BEAM

according to ETA-06/0138

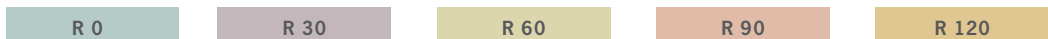
ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011



Minimum panel thickness for a specific load-span-combination

| Permanent load | Snow load on roof | SPAN OF SINGLE-SPAN BEAM l | | | | | |
|----------------------|----------------------|------------------------------|-----------|------------|------------|------------|------------|
| | | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | |
| $g_{2,k}$ | $s = \mu \cdot s_k$ | | | | | | |
| [kN/m ²] | [kN/m ²] | | | | | | |
| 0,50 | 1,00 | 3s 60 TL | 3s 80 TL | 3s 100 TL | 3s 120 TL | 5s 140 TL | |
| | 2,00 | 3s 80 TL | 3s 90 TL | 3s 120 TL | 5s 140 TL | 5s 160 TL | |
| | 3,00 | | 3s 100 TL | 5s 130 TL | 5s 150 TL | 5s 180 TL | |
| | 4,00 | 3s 90 TL | 3s 110 TL | 5s 140 TL | 5s 170 TL | 5s 200 TL | |
| | 5,00 | | 3s 120 TL | 5s 150 TL | 5s 180 TL | 7ss 220 TL | |
| | 6,00 | | 5s 130 TL | 5s 160 TL | 5s 200 TL | | |
| | 7,00 | 3s 100 TL | 5s 140 TL | 5s 170 TL | 7ss 200 TL | 7ss 240 TL | |
| 1,00 | 1,00 | 3s 80 TL | 3s 90 TL | 3s 100 TL | 5s 140 TL | 5s 160 TL | |
| | 2,00 | | 3s 100 TL | 3s 120 TL | 5s 150 TL | 5s 180 TL | |
| | 3,00 | 3s 90 TL | 3s 110 TL | 5s 140 TL | 5s 160 TL | 5s 200 TL | |
| | 4,00 | | 3s 120 TL | 5s 150 TL | 5s 180 TL | 7ss 200 TL | |
| | 5,00 | | 5s 160 TL | 5s 190 TL | 7ss 220 TL | | |
| | 6,00 | 3s 100 TL | 5s 140 TL | 5s 170 TL | | 7ss 200 TL | |
| | 7,00 | 3s 110 TL | 5s 180 TL | 7ss 200 TL | 7ss 240 TL | | |
| | 5s 140 TL | | 5s 180 TL | 7ss 210 TL | | | |
| 1,50 | 1,00 | 3s 80 TL | 3s 90 TL | 3s 120 TL | 5s 150 TL | 5s 180 TL | |
| | 2,00 | | 3s 100 TL | 5s 130 TL | 5s 160 TL | 5s 190 TL | |
| | 3,00 | 3s 90 TL | 3s 110 TL | 5s 140 TL | 5s 170 TL | 5s 200 TL | |
| | 4,00 | | 3s 120 TL | 5s 150 TL | 5s 180 TL | 7ss 220 TL | |
| | 5,00 | | 5s 130 TL | 5s 160 TL | 5s 200 TL | | |
| | 6,00 | 3s 100 TL | 5s 140 TL | 5s 170 TL | 7ss 200 TL | 7ss 240 TL | |
| | 7,00 | 3s 110 TL | 5s 180 TL | 7ss 200 TL | 7ss 210 TL | | |
| | 5s 140 TL | | 5s 180 TL | 7ss 210 TL | | | |
| 2,00 | 1,00 | 3s 80 TL | 3s 100 TL | 5s 130 TL | 5s 160 TL | 5s 200 TL | |
| | 2,00 | | 3s 110 TL | 5s 140 TL | 5s 170 TL | | |
| | 3,00 | 3s 90 TL | 3s 120 TL | 5s 150 TL | 5s 180 TL | 7ss 200 TL | |
| | 4,00 | | 3s 100 TL | 5s 140 TL | 5s 160 TL | 5s 200 TL | 7ss 220 TL |
| | 5,00 | | | | 5s 170 TL | 7ss 200 TL | |
| | 6,00 | 3s 110 TL | 5s 180 TL | 7ss 200 TL | 7ss 210 TL | 7ss 240 TL | |
| | 7,00 | | | | 7ss 210 TL | | |
| 2,50 | 1,00 | 3s 80 TL | 3s 110 TL | 5s 140 TL | 5s 170 TL | 7ss 200 TL | |
| | 2,00 | | 3s 120 TL | 5s 150 TL | 5s 180 TL | | |
| | 3,00 | 3s 90 TL | 3s 100 TL | 5s 130 TL | 5s 160 TL | 5s 190 TL | 7ss 220 TL |
| | 4,00 | | | 5s 140 TL | 5s 170 TL | 7ss 200 TL | |
| | 5,00 | | | 5s 180 TL | 7ss 200 TL | 7ss 240 TL | |
| | 6,00 | 3s 110 TL | 5s 150 TL | 5s 180 TL | 7ss 220 TL | | |
| | 7,00 | | | 5s 190 TL | 7ss 220 TL | | |



STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$k_{def} = 0,6$

Snow load at an altitude ≤ 1000 m above sea level ($\psi_0 = 0,5$ and $\psi_2 = 0,0$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Maximum roof inclination 15°

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fin} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fin} \leq \ell/250$

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

STRUCTURAL PRE-ANALYSIS TABLES

07 KLH® AS A ROOF - DOUBLE SPAN BEAM

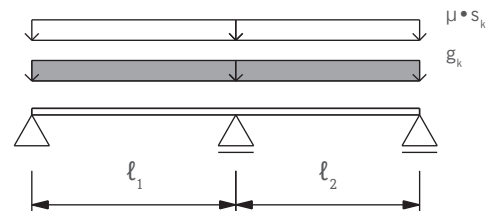
according to ETA-06/0138

ÖNORM EN 1995-1-1:2019 and ÖNORM B 1995-1-1:2019

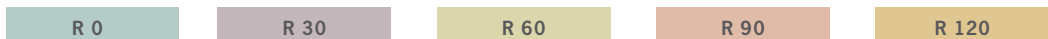
ÖNORM EN 1995-1-2:2011 and ÖNORM B 1995-1-2:2011

Snow load evenly distributed on both spans

Minimum panel thickness for a specific load-span-combination



| Permanent load $g_{2,k}$ [kN/m ²] | Snow load on roof $s = \mu \cdot s_k$ [kN/m ²] | SPAN OF DOUBLE-SPAN BEAM l_1 | | | | | $l_2 = 0,8 \cdot l_1$ to $1,0 \cdot l_1$ | | | | | |
|-----------------------------------------------------|------------------------------------------------------------------|--------------------------------|-----------|-----------|-----------|-----------|------------------------------------------|--------|--------|--------|------------|------------|
| | | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | 3,00 m | 4,00 m | 5,00 m | 6,00 m | 7,00 m | |
| 0,50 | 1,00 | | 3s 60 TL | 3s 80 TL | 3s 100 TL | 3s 120 TL | 3s 100 TL | | | | 3s 100 TL | 3s 120 TL |
| | 2,00 | 3s 60 TL | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 100 TL | | | | 3s 120 TL | 5s 140 TL |
| | 3,00 | | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 140 TL | 5s 150 TL |
| | 4,00 | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | | 5s 140 TL | | | | 5s 150 TL | 5s 170 TL |
| | 5,00 | | 3s 100 TL | 3s 110 TL | 3s 120 TL | | 5s 140 TL | | | | 5s 170 TL | 5s 200 TL |
| | 6,00 | 3s 80 TL | 3s 100 TL | 5s 140 TL | 5s 150 TL | 5s 170 TL | 5s 150 TL | | | | 5s 200 TL | 7ss 200 TL |
| | 7,00 | | 3s 110 TL | 5s 140 TL | 5s 160 TL | 5s 180 TL | 5s 170 TL | | | | 7ss 200 TL | |
| 1,00 | 1,00 | | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 100 TL | | | | 3s 120 TL | 5s 130 TL |
| | 2,00 | 3s 60 TL | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 110 TL | | | | 5s 130 TL | 5s 140 TL |
| | 3,00 | | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 140 TL | 5s 150 TL |
| | 4,00 | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 160 TL | 5s 170 TL |
| | 5,00 | | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 180 TL | 5s 180 TL |
| | 6,00 | 3s 80 TL | 3s 100 TL | 5s 140 TL | 5s 150 TL | 5s 160 TL | 5s 150 TL | | | | 5s 180 TL | 7ss 200 TL |
| | 7,00 | | 3s 110 TL | 5s 140 TL | 5s 160 TL | 5s 180 TL | 5s 160 TL | | | | 7ss 200 TL | |
| 1,50 | 1,00 | | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 110 TL | | | | 5s 130 TL | 5s 130 TL |
| | 2,00 | 3s 60 TL | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 140 TL | 5s 140 TL |
| | 3,00 | | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 150 TL | 5s 150 TL |
| | 4,00 | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 170 TL | 5s 170 TL |
| | 5,00 | | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 190 TL | 5s 190 TL |
| | 6,00 | 3s 80 TL | 3s 100 TL | 5s 140 TL | 5s 150 TL | 5s 160 TL | 5s 150 TL | | | | 5s 190 TL | 7ss 200 TL |
| | 7,00 | | 3s 120 TL | 5s 140 TL | 5s 160 TL | 5s 180 TL | 5s 170 TL | | | | 7ss 200 TL | |
| 2,00 | 1,00 | | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 140 TL | 5s 140 TL |
| | 2,00 | 3s 60 TL | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 160 TL | 5s 160 TL |
| | 3,00 | | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 180 TL | 5s 180 TL |
| | 4,00 | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 180 TL | 7ss 200 TL |
| | 5,00 | 3s 80 TL | 3s 100 TL | 5s 140 TL | 5s 150 TL | 5s 160 TL | 5s 150 TL | | | | 7ss 200 TL | |
| | 6,00 | | 3s 110 TL | 5s 140 TL | 5s 160 TL | 5s 180 TL | 5s 160 TL | | | | | |
| | 7,00 | 3s 90 TL | 3s 120 TL | 5s 150 TL | 5s 170 TL | 5s 190 TL | 5s 170 TL | | | | | |
| 2,50 | 1,00 | | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 150 TL | 5s 150 TL |
| | 2,00 | 3s 60 TL | 3s 80 TL | 3s 100 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | | | | 5s 160 TL | 5s 160 TL |
| | 3,00 | | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 170 TL | 5s 170 TL |
| | 4,00 | 3s 70 TL | 3s 90 TL | 3s 110 TL | 3s 120 TL | 3s 120 TL | 3s 120 TL | | | | 5s 190 TL | 5s 190 TL |
| | 5,00 | 3s 80 TL | 3s 100 TL | 5s 140 TL | 5s 150 TL | 5s 160 TL | 5s 150 TL | | | | 7ss 200 TL | 7ss 200 TL |
| | 6,00 | | 3s 110 TL | 5s 140 TL | 5s 160 TL | 5s 180 TL | 5s 160 TL | | | | | |
| | 7,00 | 3s 90 TL | 3s 120 TL | 5s 150 TL | 5s 170 TL | 5s 190 TL | 5s 170 TL | | | | | |



STRUCTURAL PRE-ANALYSIS TABLES

Service class 1

$k_{def} = 0,6$

Snow load at an altitude ≤ 1000 m above sea level ($\psi_0 = 0,5$ and $\psi_2 = 0,0$): $k_{mod} = 0,9$

Self-weight of KLH® is already taken into account in the table.

Maximum roof inclination 15°

Deflection limits according to ÖNORM EN 1995-1-1:2019

a) characteristic design situation: $w_{Q,inst} \leq \ell/300$ and $(w_{fn} - w_{G,inst}) \leq \ell/200$

b) quasi-permanent structural design situation: $w_{fn} \leq \ell/250$

Load-bearing capacity

a) verification of bending resistance

b) verification of shear resistance

Structural fire design (single-sided fire exposure)

Application of KLHdesigner based on the „reduced properties method“ according to ETA-06/0138.

a) charring rate $\beta_1 = 0,65$ mm/min regular charring rate (charring within one single layer)

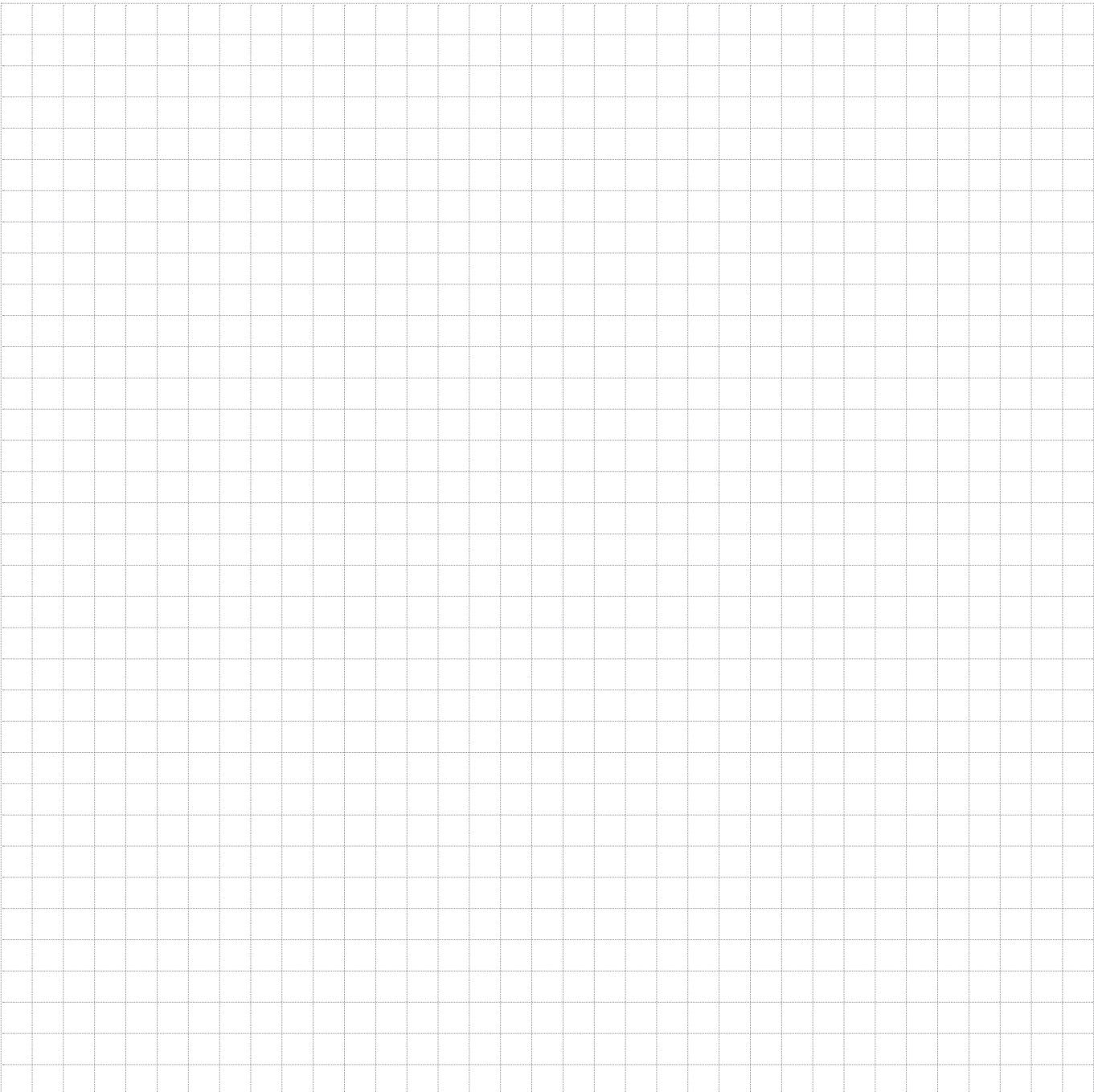
b) charring rate $\beta_2 = 1,00$ mm/min increased charring rate (after the failure / falling off of one layer)

c) for local panel parts $b < 300$ mm higher charring rates are mandatory

d) the minimum panel thicknesses (for R 0) automatically reach fire resistance according to coloured marking

This table is only intended for structural pre-analysis purposes and does not replace necessary static calculations!

NOTES

A large, empty grid of small squares, typical of graph paper or a ledger. The grid is composed of approximately 20 columns and 40 rows, with thin, light gray lines forming the boundaries of each cell.



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